

# Solitary Burnup Wave Solution in a Multi-Group Diffusion-Burnup Coupled System

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## General Background

### Well-known Figures and Facts:

- ❑ 1 kg  $^{235}\text{U}$  fission reaction produces 23 million kWh.
- ❑ Natural uranium possesses only 0.7 %  $^{235}\text{U}$  and 99.2%  $^{238}\text{U}$ . Fuel enrichment is normally needed
- ❑ Conventional light water reactors can only consume 2-5% heavy isotopes ( $^{235}\text{U}$ ,  $^{238}\text{U}$ ,  $^{239}\text{Pu}$  ...). Fast breeder reactors about 10% av. burnup. Fuel reprocessing is needed.

### Conventional Nuclear Reactors :

- ❑ **Low fuel utilization and high amount of nuclear waste due to the low burn-up**



## Burning Wave Fission Reactor: **CANDLE**

### Main features of this concept :

- ❑ Long core or continuous fuel loading
- ❑ Stable nuclear reaction (**constant reactivity**)
- ❑ High burn-up (up to 50 %) (**high utilization of fuel**)
- ❑ Natural uranium fuel (**no need of fuel enrichment**)
- ❑ Less nuclear waste (**no need of fuel reprocessing**)

### Purpose of this study :

- ❑ Setup of simplified multi-group model
- ❑ Analytical/numerical solution
- ❑ Insight into this phenomenon



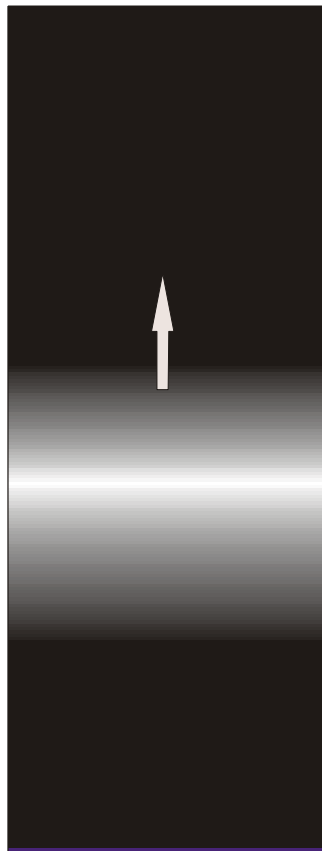
## Literature:

- ❑ Feoktistov (1989), Teller *et al.* (ICENES'96, Obninsk)
- ❑ Sekimoto *et al.* (2000, 2001, 2002, 2005)
- ❑ Van Dam (2000)
- ❑ Seifritz (2000, 2005)
- ❑ Chen *et al.* (2005, 2006)

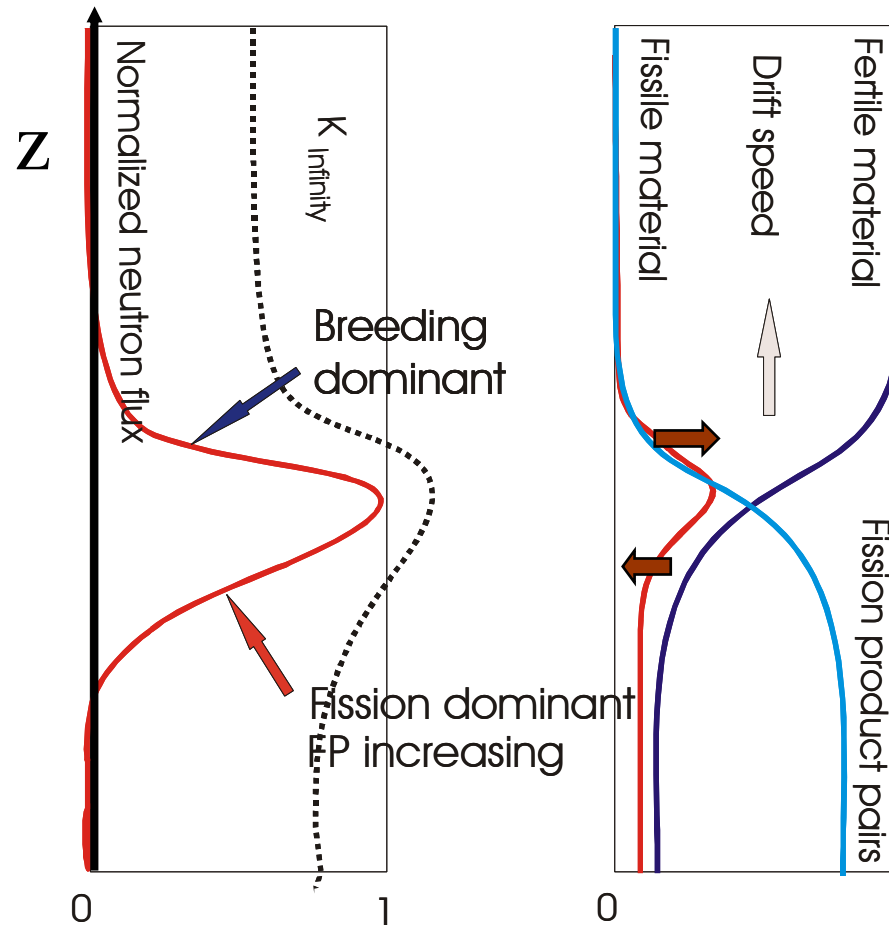
This paper attempts to apply the analytical method to the more complicated multi-group model



# Mechanism of this new kind of reactor



Ignition from bottom



Fresh fuel:  
fertile fuel

Spent fuel+FPs



## Neutronic Model (1)

Two-group diffusion equations (**fast group 1; slow group 2**):

$$\frac{1}{v_1} \frac{\partial \phi_1}{\partial t} = \nabla \cdot (D_1 \nabla \phi_1) - \Sigma_{a1} \phi_1 - \Sigma_{1 \rightarrow 2} \phi_1 + \nu_1 \Sigma_{f1} \phi_1 + \nu_2 \Sigma_{f2} \phi_2,$$

$$\frac{1}{v_2} \frac{\partial \phi_2}{\partial t} = \nabla \cdot (D_2 \nabla \phi_2) - \Sigma_{a2} \phi_2 + \Sigma_{1 \rightarrow 2} \phi_1,$$

One-group diffusion equations is derived as:

$$\frac{1}{v} \frac{\partial \phi}{\partial t} = \nabla \cdot (D \nabla \phi) - \Sigma_a \phi + \nu \Sigma_f \phi,$$

where, e.g.

$$D \nabla \phi = D_1 \nabla \phi_1 + D_2 \nabla \phi_2$$

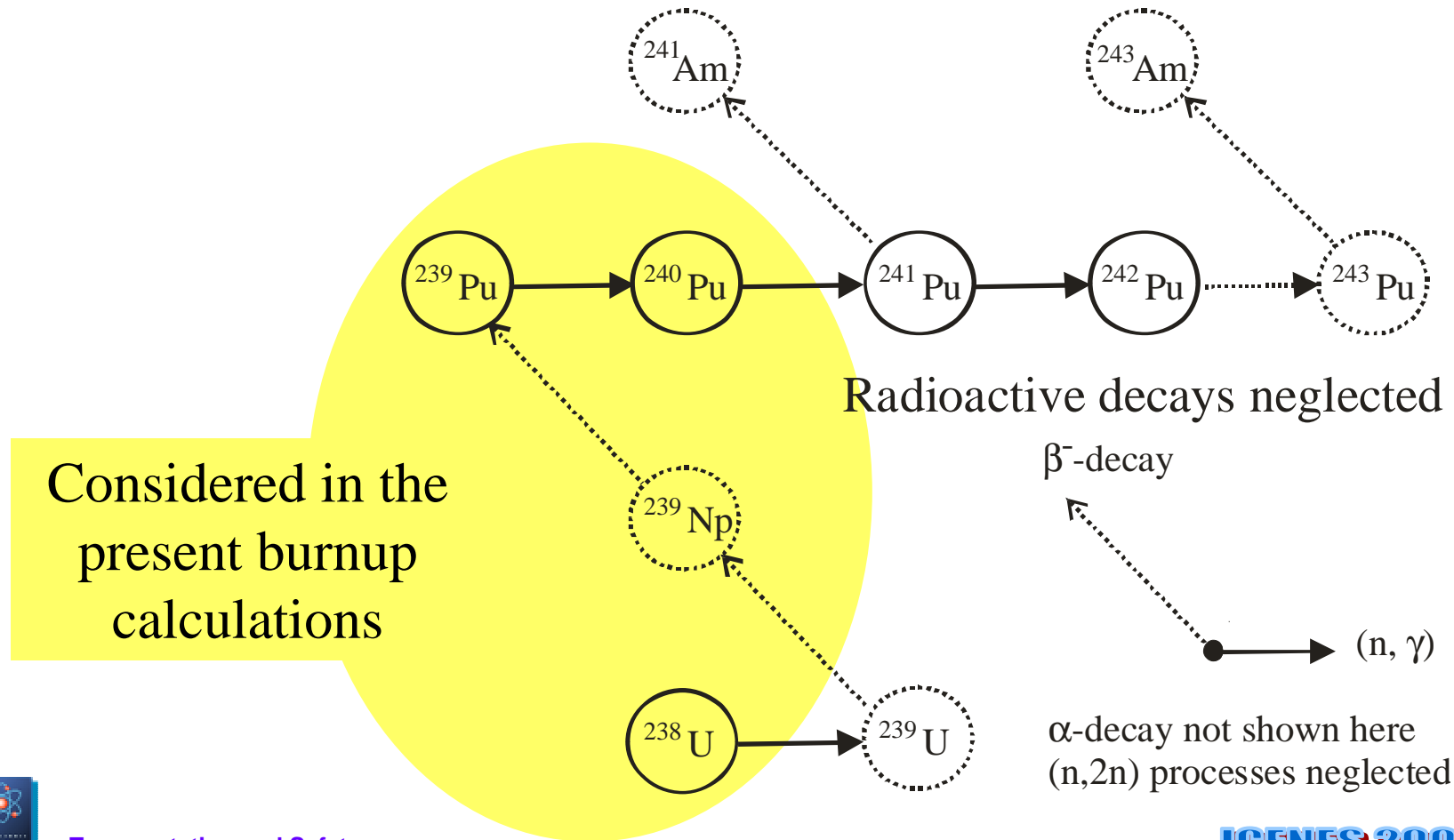
$$\Sigma \phi = \Sigma_1 \phi_1 + \Sigma_2 \phi_2$$

$$\phi = \phi_1 + \phi_2$$



# Neutronic Model (2)

## Simplified Nuclide Chain Scheme



Considered in the  
present burnup  
calculations

Radioactive decays neglected

$\beta^-$ -decay

$(n, \gamma)$

$\alpha$ -decay not shown here  
 $(n, 2n)$  processes neglected



## Neutronic Model (3)

Burn-up equations simplified by considering  $^{238}\text{U}$ ,  $^{239}\text{Pu}$ ,  $^{240}\text{Pu}$ , and burnable and non-burnable fission product pairs (FPPs) and by neglecting radioactive decay processes

$$\frac{\partial N_8}{\partial t} = -N_8 \sigma_{a,8} \phi, \quad \frac{\partial N_9}{\partial t} = -N_9 \sigma_{a,9} \phi + N_8 \sigma_{c,8} \phi, \quad \frac{\partial N_0}{\partial t} = -N_0 \sigma_{a,0} \phi + N_9 \sigma_{c,9} \phi,$$

$$\frac{\partial N_{FPP\_burn}}{\partial t} = -N_{FPP\_burn} \sigma_{a,FPP} \phi + \sum_{i=8,9,0} N_i \sigma_{f,i} \phi, \quad \frac{\partial N_{FPP\_inert}}{\partial t} = N_{FPP\_burn} \sigma_{a,FPP} \phi$$

where all  $\sigma\phi$  stands for  $\sigma_1\phi_1 + \sigma_2\phi_2$

Coupling through macroscopic cross-sections

$$\Sigma_{a,n} = \sum_i N_i (\sigma_{a,i})_n, \quad \nu\Sigma_{f,n} = \sum_i N_i (\nu_i \sigma_{f,i})_n, \quad \Sigma_{tr,n} = \sum_i N_i (\sigma_{tr,i})_n, \quad \Sigma_{1 \rightarrow 2} = \sum_i N_i \sigma_{1 \rightarrow 2,i}$$



# Asymptotic Solution

## Solutions of Burn-up equations

Atom number densities are functions of *neutron fluence*  $\psi$  only

$$N_i = N_i(\psi), \quad \psi = \int_{t_0}^t \phi \, dt = \psi_1 + \psi_2$$

Asymptotic Formulation in  $\zeta = z + ut$

Look for a so-called travelling wave solution with drift speed  $u$ , *i.e.* a steady solution in a moving coordinate system  $O\zeta$  in 1-D case

$$\frac{\partial}{\partial \zeta} \left( D \frac{\partial}{\partial \zeta} \phi \right) - \Sigma_a \phi + \frac{v \Sigma_f}{k_{eff}} \phi = 0, \quad \frac{\partial}{\partial \zeta} \left( D_2 \frac{\partial}{\partial \zeta} \phi_2 \right) - (\Sigma_{a2} + \Sigma_{1 \rightarrow 2}) \phi_2 + \Sigma_{1 \rightarrow 2} \phi = 0.$$

↓  
 $\phi$ -equation

↓  
 $\phi_2$ -equation



## Iterative Solution Method

The analytical solvability of one-group equation (Chen *et al.* ICENES 2005), i.e. if  $\Sigma_a(\psi)$ ,  $\Sigma_f(\psi)$  and  $D(\psi)$  are known, the  $\phi$ -equation can be solved analytically, where  $\psi = \int \phi d\zeta / u$

The two-group equations can be solved **iteratively** based on this one group solution:

(1) Select a suitable constant  $\alpha^{(0)} = \phi_2 / \phi$ , an analytical solution of  $\phi$ -equation and a numerical solution of  $\phi_2$ -equation are obtained

(2) Then  $\alpha^{(1)}(\psi) = \phi_2^{(1)}(\psi) / \phi^{(1)}(\psi) \implies k_{eff}^{(2)}, \phi^{(2)}(\psi)$  and  $\phi_2^{(2)}(\psi)$

(3)  $\alpha^{(n)}(\psi) = \phi_2^{(n)}(\psi) / \phi^{(n)}(\psi) \implies k_{eff}^{(n+1)}, \phi^{(n+1)}(\psi)$  and  $\phi_2^{(n+1)}(\psi)$

If  $\alpha^{(n)}$  is sufficiently close to  $\alpha^{(n-1)}$ , we say, a converged solution has been achieved



## Example

- Material composition similar to that in a “simplified standard system” (**sodium-cooled fast breeder reactor** with oxide fuel)
- Two-group data have been generated with boundary 111keV.
- Fresh fuel parameters:

$$\sigma_{a,0} = 0.528 \text{ barn}$$

$$N_{8,0} + N_{9,0} = 6.32 \times 10^{21} \text{ cm}^{-3}$$

$$D_0 = 1.556 \text{ cm}$$

$$N_{9,0} / (N_{8,0} + N_{9,0}) = 0.065663$$

- Maximal neutron flux is chosen as  $\phi_{\max} = 3 \times 10^{15} \text{ cm}^{-2} \text{ s}^{-1}$
- Derived scales

$$l_0 = 21.6 \text{ cm}$$

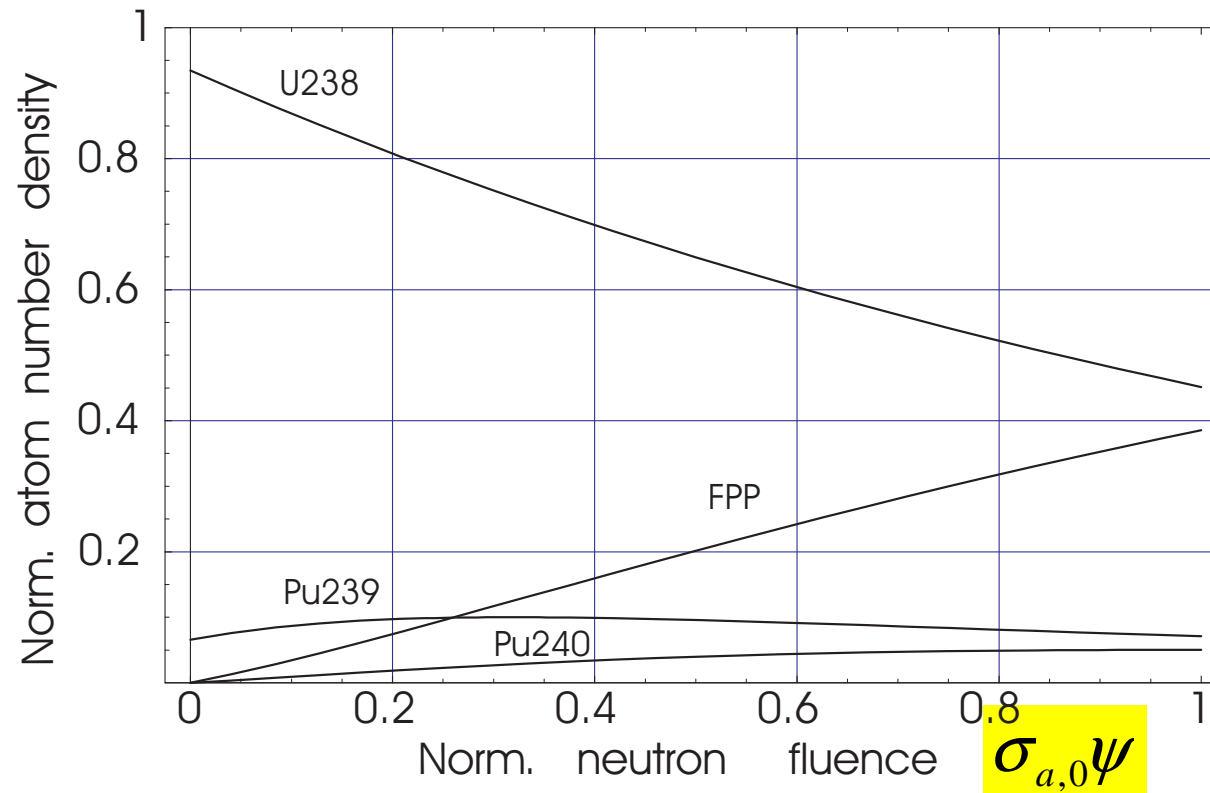
$$u_0 = 3.42 \times 10^{-8} \text{ cm/s}$$

$$\text{for } Z = \zeta / l_0, \quad U = u / u_0$$



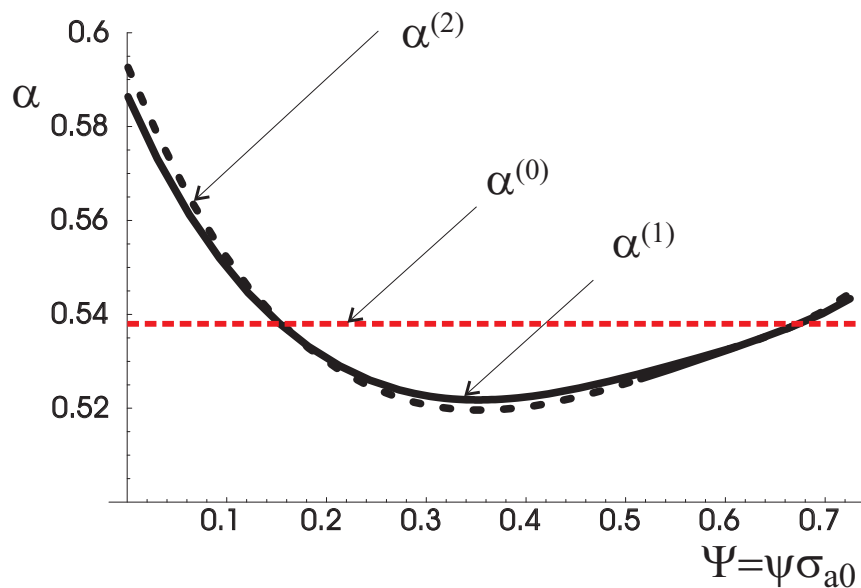
## Results (1)

- A typical burn-up solution in the case of constant microscopic cross sections

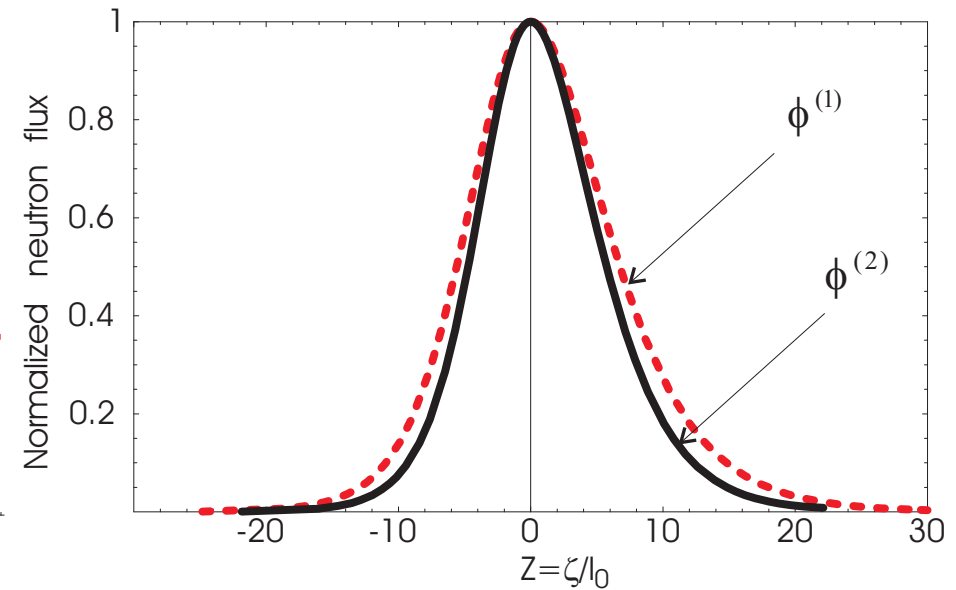


## Results (2)

- Comparison of one-group and two-group solutions



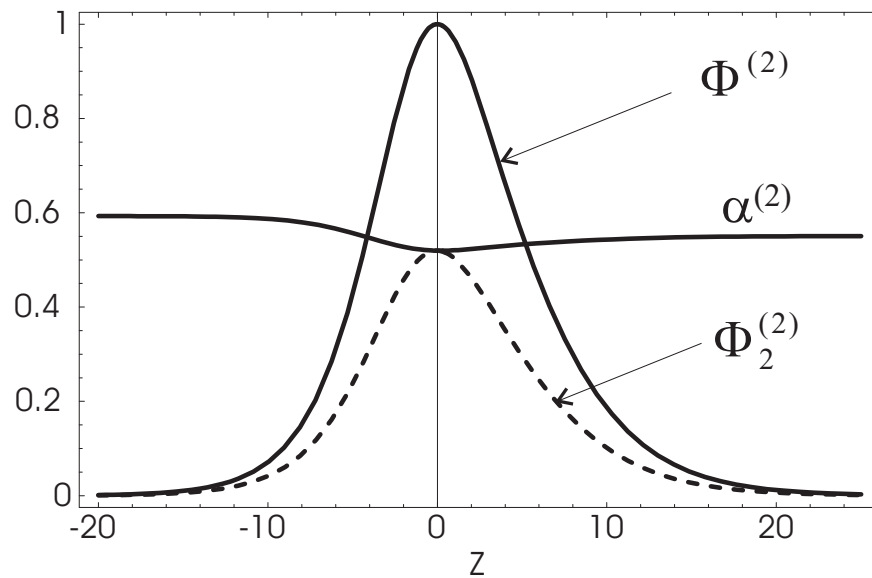
Flux fraction of slow group



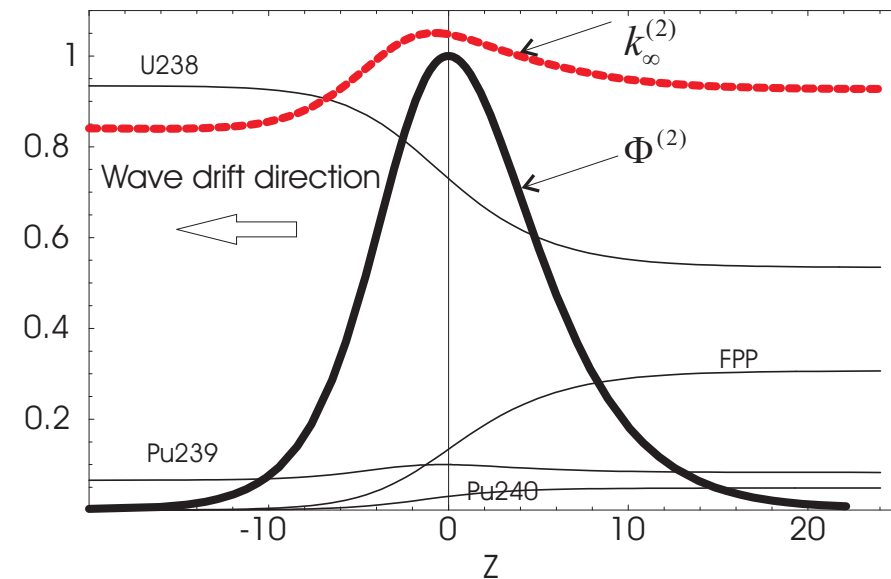
Total neutron flux

## Results (3)

- Summary of the two-group solution



Slow neutron flux fraction



2-group solution summary

- The drift speed is 16.7 cm/year and the Z-range of (-20,20) corresponds 8.64 m



## Conclusions

- ❑ Two-group diffusion equations coupled with simplified burn-up equations were investigated for a CANDLE-type reactor.
- ❑ In the 1-D case the model was solved by the iterative method based on the analytical solvability of one-group theory.
- ❑ It was shown that the fraction of slow neutron flux changes slightly in the wave solution and consequently the iteration converges very quickly.
- ❑ The method can be further developed for a more complicated multi-group model with a large number of energy groups, to obtain a so-called “**fundamental burning wave solution**”.

